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DESIGN AND FABRICATION OF HELMET BY HYBRID COMPOSITE

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ABSTRACT

In this work structural strength analysis is carried out in the Composite Helmet by Using Coconut fiber and Glass Fiber .In this recent world the fiber strengthened composite materials are synthesized using glass fiber as reinforcements together with matrix, which have attracted the attention of researchers due to their low density with high specific mechanical strengths, convenience ,and renewability. The current work efforts to make a development in the current existing helmet manufacturing procedure and materials used to have better mechanical properties as well as to enhance the compatibility between fiber sand the matrix. The composites are ready with the unsaturated polyester matrix and fibers such as, reinforced composite materials and glass fiber using hand lay-up method with suitable proportions to result in helmet shell construction. The fabricated helmet are planned to analyze through Finite element method estimate its mechanical properties such as Deformation and stress failure.

Key Words:

Coconut fiber

Epoxy risen

Glass fiber

Finite Element Analysis

1. INTRODUCTION:

All helmets attempt to protect the user's head by absorbing mechanical energy and protecting against penetration. Their structure and protective capacity are altered in high-energy impacts. Beside their energy absorption capability, their volume and weight are also important issues, since higher volume and weight increase the injury risk for the user's head and neck. Every year many workers are killed or seriously injured in the construction, manufacturing and power industry because of head injuries. Wearing an appropriate safety helmet significantly reduces the risk of injury or even death. Protective headwear could save your life. At present strength of the helmet using industry is less due to improper selection and filling of material, uneven pressure distribution and blow holes. The aim of the project is to increase the strength of industrial helmet shell by using composite material. The safety helmet selected should satisfy certain Performance requirements including shock absorption, resistance to penetration. To achieve this an improvement in





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shell material by using composite material will be studied in this project.

2. METHODOLOGY

Selection of Matrix Material Epoxy LY-556 (diglycidal ether of Bisphenol-A, DGEBA, with a density of 1.16 gm/cm^3) was chosen as the matrix material, belonging to the Epoxide family. HY 951, a triethylene tetra-amine with a density of 0.95 gm/cm^3 , was used as the hardener. Both materials were sourced from Araldite Industrial Adhesives Selection of Reinforcement and Natural Fibers Natural fibers, including Sisal and Jute, were selected as reinforcements for the polymer composite. Additionally, Glass fiber (7 mil, 200 ± 20 GSM) was chosen as a synthetic fiber for reinforcement. Availability of Natural Fiber (Sisal & Jute) 0.7mm Thickness Sisal (Agave sisalana) is a biodegradable and renewable natural fiber commonly used in twine and rope production. Coconut fiberclothis durable. low-maintenance, and resistant to wear and tear. Availability of Synthetic Fiber Glass fiber cloth (7 mil & 200 ± 20 GSM) was sourced from TEXPLAS INDIA PVT. LTD. (Haridwar) Fiberglass is known for its strength, corrosion resistance, moldability, and costeffectiveness, making it ideal for composite applications. Its non-conductive and radio frequency transparent properties are beneficial in electronics housing Surface Treatment of Fibers .To improve fiber-matrix bonding, the natural fibers were treated with a 5% NaOH solution for 3-4 hours to remove impurities. After treatment, the fibers were dried under sunlight for 1-2 hours. Wet Hand Lay-up Technique The wet hand lay-up technique was used for composite processing. A release gel was applied to the mold surface to prevent polymer sticking. Thin plastic sheets were used for a good surface finish. Woven mats or chopped strand mats were cut and placed on the mold surface, followed by pouring a mixture of thermosetting polymer and hardener. Each layer of polymer and reinforcement was spread and pressed to remove air and excess polymer. This process was repeated until the required layers were stacked. After curing, the composite was removed from the mold. The typical curing time for an epoxybased system is 24-48 hours at room temperature. This method is suitable for thermosetting polymerbased composites and is commonly used in aircraft, automotive parts, and other applications requiring lower production rates and cost-effective solutions.

3. MATERIAL SELECTION:

Epoxy Resin (LY-556)

Epoxy resin, specifically LY-556, is a widely used material due to its remarkable properties. It is light in weight and highly resistant to most alkalis and acids, making it an ideal choice for applications where chemical exposure is a concern. Additionally, it resists stress cracking, retains both stiffness and flexibility, and has low moisture absorption. These characteristics ensure the material maintains its structural integrity under varying conditions. Epoxy resin is non-staining and can be easily fabricated, which makes it versatile for a range of uses. Some of the primary applications of epoxy resin include structural applications, industrial tooling. composites, and electrical systems or electronics. Its resilience and adaptability make it an essential material in industries where durability and reliability are crucial.

Hardener (HY-951)

The hardener (HY-951) is a key component in the epoxy resin curing process. This curing agent, often referred to as a catalyst, is necessary to initiate the hardening of the epoxy resin. Without the hardener, the resin would remain in a liquid or semi-solid form and would not achieve the desired solid and durable state. The selection of an appropriate hardener is crucial, as it influences the final characteristics of the epoxy composite, such as its hardness, flexibility, and overall strength. The combination of epoxy resin and hardener determines the final properties of the composite, ensuring it meets the specific requirements of the intended application.

Natural Fibers (Coconut Fiber) and Synthetic Fibers (Glass Fiber Cloth)

Fiber-reinforced polymer composites are a critical category of materials used across various industries due to their high specific strength and modulus. Traditional fiber-reinforced plastics, often made with glass, carbon, or aramid fibers, are facing increasing scrutiny because of their environmental impact. The production, use, and disposal of these synthetic fibers are contributing to environmental concerns. In



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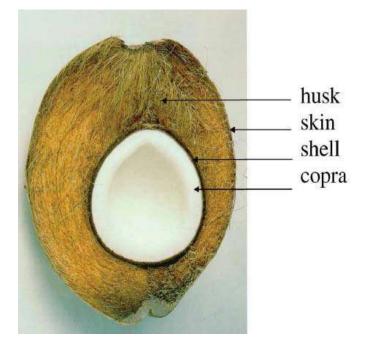


response, natural fiber composites have emerged as a sustainable alternative. These composites use fibers, particles, or platelets derived from renewable resources, such as coconut fiber. Unlike synthetic fibers, these natural fibers are biodegradable and non-toxic, offering a more eco-friendly option for reinforcing polymer composites.

Advantages of Natural Fibers

When compared to conventional reinforcing fibers like glass, carbon, and Kevlar, natural fibers offer several key advantages that make them a preferable choice in various applications. Notably, natural fibers are environmentally friendly, as they are fully biodegradable, unlike synthetic fibers that persist in the environment for long periods. They are non-toxic, making them safer for both the environment and human health. Furthermore, natural fibers often come from renewable sources, offering an inherently sustainable option for the production of composite materials. These properties make natural fibers an attractive choice for industries looking to reduce their environmental footprint while still achieving high-performance material characteristics.

In summary, the materials used in this work—epoxy resin, hardener, synthetic fibers, and natural fibers play a crucial role in the development of composites with specific mechanical properties. The combination of these materials allows for the creation of composites that are durable, environmentally friendly, and suitable for a wide range of applications.



4. DESIGN MODELING:

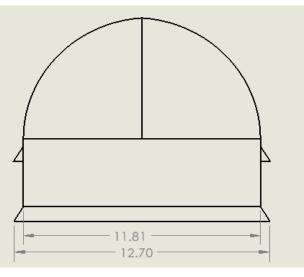
The helmet is designed for lightweight, high impact resistance, and ergonomic comfort. The outer shell consists of E-glass fiber-reinforced epoxy for strength, while coconut fiber layers enhance shock absorption. 3D modeling is performed using SolidWorks, ensuring an aerodynamic shape and proper head fit. Finite Element Analysis (FEA) in ANSYS evaluates stress distribution and impact resistance. The layering sequence is optimized for maximum energy dissipation. Thickness variations reinforce high-impact zones, ensuring safety. Ventilation and padding improve wearability. This hybrid composite approach aims to enhance sustainability and performance over conventional helmets.

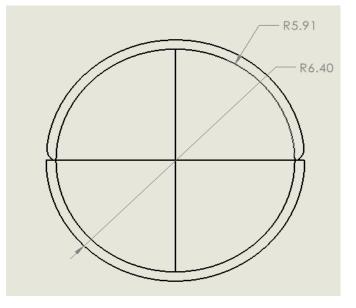
ITEM NO.	PART NUMBER	DESCRIPTION	QTY.
1 Surface_helmet		Coconut fiber, epoxy risen, glass fiber	1

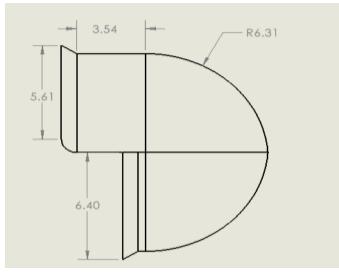




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5. FEA ANALYSIS: INTRODUCTION OF FINITE ELEMENT SOFTWARE

The Basic concept in FEA is that the body or structure may be divided into smaller elements of finite dimensions called "Finite Elements". The original body or the structure is then considered as an assemblage of these elements connected at a finite number of joints called "Nodes" or "Nodal Points". Simple functions are chosen to approximate the displacements over each finite element. Such assumed functions are called "shape functions". This will represent the displacement within the element in terms of the displacement at the nodes of the element. Mathematically, the structure to be analyzed is subdivided into a mesh of finite sized elements of simple shape. Within each element, the variation of displacement is assumed to be determined by simple polynomial shape functions and nodal displacements. Equations for the strains and stresses are developed in terms of the unknown nodal displacements. From this, the equations of equilibrium are assembled in a matrix form which can be easily be programmed and solved in software. After applying the appropriate boundary conditions, the nodal displacements are found by solving the matrix stiffness equation. Once the nodal displacements are known, element stresses and strains can be calculated.

4.1ANSYS

ANSYS is general-purpose finite element analysis (FEA) software package. Finite Element Analysis is a numerical method of deconstructing a complex system into very small pieces (of userdesignated size) called elements. The software implements equations that govern the behaviour of these elements and solves them all; creating a comprehensive explanation of how the system acts as a whole. These results then can be presented in tabulated, or graphical forms. This type of analysis is typically used for the design and optimization of a system far too complex to analyze by hand. Systems that may fit into this category are too complex due to their geometry, scale, or governing equations. Static structural Solver

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Sizing

- A. Importing External geometry
- B. Meshing
- C. Material Properties Apply 0
- D. Boundary Condition
- E. Solveig
- F. Post processing

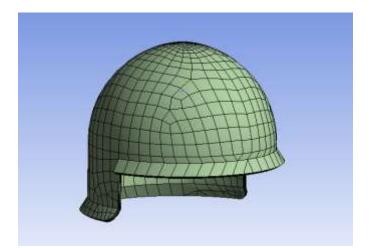
Importing External Geometry;

After preparing the model in CATIA it is improved to ANSYS. the file is imported from CATIA by file>import>STEP



4.3.3GENERATE MESHES:

For Solving purpose and boundary condition we want to generate element which was done through mesh option



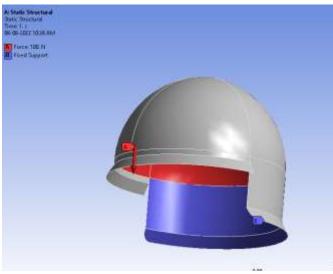
Sizing	
Use Advanced Size Function	On: Curvature
Relevance Center	Medium
Initial Size Seed	Active Assembly
Smoothing	Medium
Span Angle Center	Coarse
Curvature Normal Angle	Default (30.0 °)
Min Size	Default (4.0980 mm)
Max Face Size	Default (20.490 mm)
Growth Rate	Default
Minimum Edge Length	10.0 mm
Inflation	
Use Automatic Inflation	None
Inflation Option	Smooth Transition
Transition Ratio	0.272
Maximum Layers	2
Growth Rate	1.2
Inflation Algorithm	Pre
View Advanced Options	No
Statistics	
Nodes	754
Elements	724

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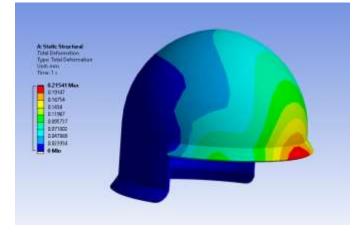


Material Data

1) Polyethylene

TABLE 15Polyethylene > Constants						
Density		9.5e-	9.5e-007 kg mm^-3			
Coefficient of Thermal Expansion		2.3e-004 C^-1				
Specific Heat	Specific Heat		2.96e+005 mJ kg^-1 C^-1			
Thermal Conducti	Thermal Conductivity		2.8e-004 W mm^-1 C^-1			
Young's Modulus MPa	Poisson's Ratio		Bulk Modulus MPa	Shear Modu MPa		
	1100		0.42	2291.	.7	387.32

Deformation:



Total deformation of helmet

Elastic strain

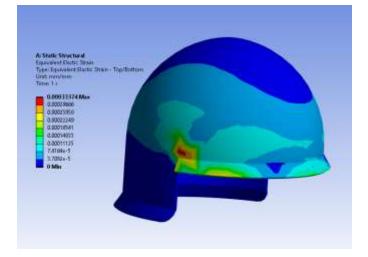
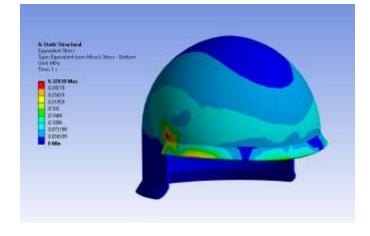


Fig maximum stress of in plastic helmet



COMPOSITE MATERIAL ANALYSIS IN ANSYS



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100
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Fabric Properties - Norms
General Draping Coefficients Analysis Solid Model Opc. General Moteval: Epocy I: Glass UD Trictensis 1.3 Price/Anac 0.0 Mass/Anac: En 09 Proct-Processing Ignore for Proct-Processing

Material constrain:

Material Data

2) Sisal Fibre

TABLE 22

Sisal Fibre> Constants

Density	1.45e-006 kg mm^-3
Coefficient of Thermal Expansion	1.2e-005 C^-1
Specific Heat	4.34e+005 mJ kg^-1 C^-1
Thermal Conductivity	6.05e-002 W mm^-1 C^-1
Resistivity	1.7e-004 ohm mm

TABLE 23

Sisal Fibre> Compressive Ultimate Strength

Compressive Ultimate Strength MPa

TABLE 24

Sisal Fiber> Compressive Yield Strength

0

Compressive Yield Strength	MPa
250	

TABLE 25

Sisal Fiber> Tensile Yield Strength

Tensile Yield Strength MPa

250

TABLE 26

Sisal Fiber> Tensile Ultimate Strength

Tensile Ultimate Strength MPa 460

TABLE 27

Sisal Fiber> Isotropic Secant Coefficient of Thermal Expansion

Referen	ce Temperature C
22	

TABLE 28 Sisal Fiber> Alternating Stress Mean Stress					
Alternating Stress MPa					
3999	10	0			
2827	20	0			
1896	50	0			
1413	100	0			
1069	200	0			
441	2000	0			
262	10000	0			
214	20000	0			
138	1.e+005	0			
114	2.e+005	0			
86.2	1.e+006	0			
TA	BLE 29				

TABLE 29 Sisal Fiber> Strain-Life Parameters

	Strength Coefficien t MPa	U	Ductility Coefficien t	Ductility Exponen t	Cyclic Strength Coefficien t MPa	Cyclic Strain Hardenin g Exponent
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920	-0.106	0.213	-0.47	1000	0.2

TABLE 30 Sisal Fiber> Isotropic Elasticity					

C	Modulus MPa	Ratio	Modulus MPa	Modulus MPa
	3770	0.32	3490.7	1428





3) Epoxy E-Glass UD

TABLE 32Epoxy E-Glass UD > ConstantsDensity2.e-006 kg mm^-3

TABLE 33

Epoxy E-Glass UD > Orthotropic Elasticity

	You	You	You						
	ng's	ng's	ng's				Shea	Shea	Shea
Tempe	Mod	Mod	Mod	Poiss	Poiss	Poiss	r	r	r
rature	ulus	ulus	ulus	on's	on's	on's	Mod	Mod	Mod
C	Х	Y	Z	Ratio	Ratio	Ratio	ulus	ulus	ulus
L	direc	direc	direc	XY	ΥZ	XZ	XY	ΥZ	XZ
	tion	tion	tion				МРа	МРа	MPa
	МРа	MPa	MPa						
	450	100	100	0.3	0.4	0.3	500	384	500
	00	00	00	0.5	0.4	0.5	0	6.1	0

TABLE 34
Epoxy E-Glass UD > Orthotropic Strain Limits

Tempe rature C	Tens ile X dire ction	Tens ile Y dire ction	ile Z dire	Compr essive X directi on	Compr essive Y directi on	-	Sh ea r XY	Sh ea r YZ	Sh ea r XZ
	2.44 e- 002	3.5e- 003	3.5e- 003	-1.5e- 002	-1.2e- 002	-1.2e- 002	1.6 e- 00 2	1.2 e- 00 2	1.6 e- 00 2

	Epox	y E-Gla	ass UD	> Ortho	otropic S	Stress Li	mits	5	
Tempe rature C	Tens ile X dire ctio n MPa			Compr essive X directi on MPa	Compr essive Y directi on MPa	Compr essive Z directi on MPa	Sh ea r XY M Pa	She ar YZ MP a	Sh ea r XZ M Pa
	110 0	35	35	-675	-120	-120	80	46. 15 4	80

TABLE 35

TABLE 36

Epoxy E-Glass UD > Puck Constants

Temperatur e C	-	Compressiv e Inclination YZ		Tensile Inclinatio n YZ
	0.25	0.2	0.3	0.2

TABLE 37 Epoxy E-Glass UD > Additional Puck Constants

Interface Weakening	Degradation	Degradation
Factor	Parameter s	Parameter M
0.8	0.5	

TABLE 38 Epoxy E-Glass UD > Tsai-Wu Constants

Temperature	Coupling	Coupling	Coupling
C	Coefficient XY	Coefficient YZ	Coefficient XZ
	-1	-1	





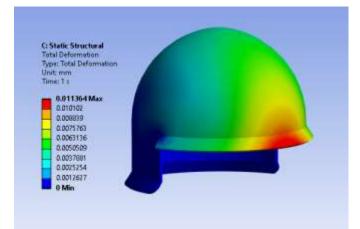
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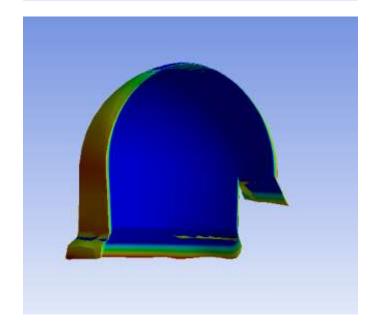
COMPOSITE

SIMULATION RESULT MATERIAL:

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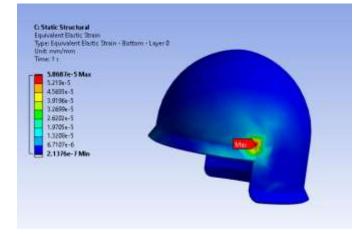
Total deformation:



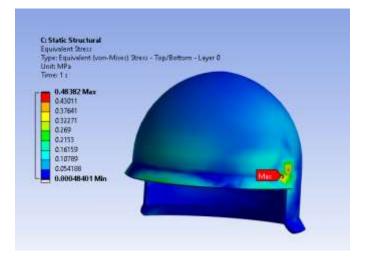


Cross sectional view of deformation

Strain of composite helmet



Equivalent stress



CONCLUSION

S.n	Material	Total	Strain	Stres
0		deformation(m		S
		m)		(MPa
)
1	Polyethyle ne	0.215	0.0003 3	0.33
2	Natural fiber	0.01136	5.57x1 0 ⁻⁵	0.48

Based on the structural analysis results, the helmet material significantly influences deformation, strain, and stress distribution. The analysis compared



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polyethylene and natural fiber composites under loading conditions: Polyethylene exhibited a total deformation of 0.215 mm, a strain of 0.00033, and a stress of 0.33 MPa. This indicates relatively higher deformation but lower stress absorption. Natural fiber composite showed significantly lower deformation at 0.01136 mm, with a strain of 5.57 × 10⁻⁵ and a higher stress of 0.48 MPa, indicating better rigidity and load-bearing capacity. The results suggest that natural fiber composites offer superior stiffness and reduced deformation compared to polyethylene, making them a promising material for impact-resistant helmet applications. However, further testing on durability, energy absorption, and long-term performance is recommended for practical implementation.

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	Area(m					-	896.45		
		im Load 90	wh.				7.04	-	
1			7						
And Tests									
Serre	ple ID	Nature of Bend	Length h (mm)	Thickne #	Width (mnt)	Mandr elDia (mm)	Angleof Bend (Deg)	Observation	
Nature	Fiber	Bevi	365	26	30	52	90"	Sample Broken	
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9. REFERENCES

- A Review On Sisal Fiber reinforced Polymer Composites. Kuruvilla Joseph1, Romildo Dias Toledo Filho2, Beena James3, Sabu Thomas4 & Laura Hecker de Carvalho5 RevistaBrasileira de EngenhariaAgrícola e Ambiental, v.3, n.3, p.367-379, 1999 Campina Grande, PB, DEAg/UFPB
- 2) Properties of SBS and Sisal Fiber Composites: Ecological Material for Shoe Manufacturing José Carlos Krause de Verney*, Martha Fogliato Santos Lima, Denise Maria Lenz
- 3) Tensile Properties and SEM Analysis of Bamboo and Glass Fiber Reinforced Epoxy Hybrid Composite Sh. Raghavendra Rao*1, A. Varada Rajulu2, G. Ramachandra Reddy3and K. Hemachandra Reddy4
- **4)** Biodegradable Polymers: Past, Present, and Future M. Kolybaba1, L.G. Tabil 1, S. Panigrahi1, W.J. Crerar1, T. Powell1, Wang1
- 5) Yan Li, Yiu-Wing Mai, Lin Ye, 'Sisal fiber and its composites: a review of recent developments'. Composites Science and Technology, volume 60, (2000), 2037-2055.
- **6)** K. Murali Mohan Rao, K. Mohana Rao 'Extraction and tensile properties of natural fibers: Vakka, date and bamboo'. Composite Structures volume 77,(2007), 288–29.
- 7) A.Alavudeen,M.Thiruchitrambalam, N.Venkateshwaran and A.Athijayamani

"Review of natural fiber reinforced Woven composite" Advances in Material science, volume - 27: 2011.

 B) H.M.M.A. Rashed, M. A. Islam and F. B. Rizvi, "EFFECTS OF PROCESS PARAMETERS ON TENSILE STRENGTH OF JUTE FIBER REINFORCEDTHERMOPLASTIC COMPOSITES",





ISSN 2581-7795

Journal of Naval Architecture and Marine Engineering, June , 2006.

- **9)** A.V.Ratna Prasad K.Murali Mohan Rao and G.Nagasrinivasulu"Mechanical properties of banana empty fruit bunch fiber reinforced polyester composites" Indian journal of fiber and textile reasearch,Vol-34:2009.
- **10)** JORG MUSSIG "Industrial Applications of Natural Fibers" Department of Biomimetics, Hochschule Bremen – University of Applied Sciences, Bremen, Germany.
- 11) Lina Herrera, SelvumPillay and UdayVaidya"Bananafiber composites for automotive and transport applications" Department of Matrial Science & Engineering, University of Alabama at Birmingham, Birmingham, AL 35294.
- 12) Belmar's H, Barrera A, Castillo E, Verheugen E, Monjaras M. New composite materials from natural hard fibers .IndEngChem Prod Res Dev 1981; 20 (3): 555-61.
- 13) Cruz-Ramos CA, Moreno Saenz E, Castro Bautista
 E. Memorias del 1er.Simposium Nacional de Poli'meros, Universidad NacionalAuto'noma deMe'xico, D.F.; 1982:153.\
- 14) Casaurang-Marti'nez MN, Peraza-Sa'nchez SR, Cruz-Ramos CA. Dissolving-grade pulps from henequen fiber. CellulChemTechnol 1990; 24: 629– 83.
- 15) Silva RV, Spinelli D, Bose Filho WW, Claro Neto S, Chierice GO, TarpaniJR.Fracture toughness of natural fibers/castor oil polyurethane composites. Compos SciTechnol 2006;66:1328–35.

- 16) IdiculaMaries, BoudenneAbderrahim, Umadevi L, Ibos Laurent, CandauYvess, ThomasSabu. Thermophysical properties of natural fibre reinforced polyester composites. Compos SciTechnol 2006; 66: 2719–25.
- 17) Panthapulakkal S, Sain M. Injection-molded short hemp fiber/glass fiber reinforced polypropylene hybrid composites – mechanical, water absorption and thermal properties. J ApplPolymSci 2007; 103: 2432–41.
- 18) Arbelaiz et al," Influence of matrix/fiber modification, fiber content, water uptake and recycling", Composites Science and Technology, 2005; 65: 1582–92.
- 19) Thwe MM, Liao. Durability of bamboo-glass fiber reinforced polymer matrix hybrid composites. Compos SciTechnol 2003; 63:375–87. Varghese S, Kuriakose B, Thomas S. Stress relaxation in short sisal fiber-reinforced natural rubber composites. J ApplPolymSci 1994; 53: 1051–60.